

PROBLEM SET 5

1.

First, we need to consider the case where the two conductors are perfect conductors. We will model the parallel plate conductors as a series of small sections of length dl and consider a section with the ends located at l and $l+dl$. The capacitance and inductance between neighboring sections of the two plates are

$$dL = \mu_0 d dl / W$$

$$dC = \epsilon_0 W dl / d$$

The change in the voltage across a section is then given by

$$V(l+dl) = V(l) - i\omega I dL$$

$$V(l+dl) - V(l) \simeq dV = -i\omega \mu_0 I d dl / W$$

$$dV / dl = -i\omega \mu_0 I / W$$

In a similar fashion, the change in the current along the length must take account of the capacitor.

$$dI = -i\omega dC V$$

$$dI / dl = -i\omega \epsilon_0 W / d$$

Simply choose one equation, take the derivative with respect to dl .

$$d^2 I / dl^2 + I \omega^2 \epsilon_0 \mu_0 = 0$$

Now we consider the case where the conductivity of one conductor is dominated by the kinetic inductance of the electrons ($\omega\tau \gg 1$). In this case

$$\sigma = (ne^2\tau / m) / (1 - i\omega\tau) \simeq ine^2 / m\omega$$

$$\rho = 1 / \sigma = -i(m / ne^2)\omega$$

Now consider the conductivity of the imperfectly conducting plate. Taking account of the number of carriers, and the width and length of the strip, we find:

$$V = I \rho dl / W = -iI(m / ne^2)\omega dl / W$$

Note the similarity to the above voltage drop associated with the inductor, particularly the ω dependence. Thus, we can lump the two terms together in our derivation of the differential equation for I .

The ordinary magnetic field inductance will be negligible when

$$(m / ne^2) \gg \mu_0$$

The characteristic impedance of the line is

$$dV / dl = -i\omega LI$$

$$dI / dl = -i\omega CV$$

$$V/I=L/C*(dI/dl)/(dV/dl)$$

However

$$dI/dl=-i\omega(LC)^{1/2}I=dV/dl(C/L)^{1/2}$$

$$V/I=(L/C)^{1/2}=\left(\frac{m/ne^2W}{\epsilon_0 W/d}\right)^{1/2}=\left(\frac{md}{ne^2\epsilon_0 W^2}\right)^{1/2}$$

2.

See the final pages for a derivation of \vec{B} and \vec{E} . Note that c in this problem has been relabeled d, and oriented along the z-axis. Then a=.5 cm, b = .5 cm, and d = 1.0 cm. For the lowest mode, n=1, and either l=1 and m=0, or l=0 and m=1 (we will choose l=1, m=0). We neglect l=0 and m=0 because it is a trivial solution.

$$\omega=\frac{c\pi}{ad}(a^2+d^2)^{1/2}$$

$$E_x=0$$

$$E_y=(iB_0\omega a/\pi)\sin(\pi x/a)\sin(\pi z/d)e^{-it\omega}$$

$$E_z=0$$

$$B_x=(-B_0a/d)\sin(\pi x/a)\cos(\pi z/d)e^{-it\omega}$$

$$B_y=0$$

$$B_z=(B_0)\cos(\pi x/a)\sin(\pi z/d)e^{-it\omega}$$

The energy stored in the mode is given by the integral of B^2 and E^2 over the entire resonator volume and average over time.

$$U=1/2\int \epsilon_0 E^*E + B^*B/\mu_0$$

$$U=(1/2)B_0^2(\epsilon_0(\frac{a\omega}{\pi})^2+(a^2/d^2+1)/(\mu_0))*(abd/4)$$

$$U=(1/2)B_0^2(\epsilon_0c^2\frac{a^2+d^2}{d^2}+(a^2/d^2+1)/(\mu_0))*(abd/4)$$

$$U=(1/2)abdB_0^2(\frac{a^2+d^2}{d^2})/(\mu_0)$$

As per the class notes, the energy loss at a conducting surface is given by

$$\vec{J}\cdot\vec{E}=K^2/(\delta^2\sigma)$$

$$\delta\simeq(2/\mu_0\omega\sigma)^{1/2}$$

$$\vec{K}\times\hat{n}=\vec{B}/\mu_0$$

To consider the loss in the cavity, we must consider the surfaces with a parallel magnetic field; in this case, x=0, x=a, y=0, y=b, z=0, and z=d. We need to average the over the entire area of each side, up to the penetration depth, and over time as well.

I. x=0,a

$$\int K^2=\int B_z^2/\mu_0=B_0^2bd\delta/4$$

$$\vec{J}\cdot\vec{E}=K^2/(\delta^2\sigma)=(B_0^2bd/4\mu_0\sigma\delta)$$

For 2 sides, the power dissipated will be doubled.

$$P_x = (B_0/(\mu))^2 bd / 2\mu\sigma\delta$$

II. $y=0, b$

We need to perform similar calculation as above, except accounting for both B_z and B_x . The result is

$$P_y = (B_0/(\mu))^2 ad / 2\mu\sigma\delta (1 + (a^2)/(d^2))$$

III. $z=0, d$

We solely need to account for B_x .

$$P_z = ((B_0/(\mu))^2 ab / 2\mu\sigma\delta) (a^2)/(d^2)$$

The total power dissipated is then

$$P_t = (B_0^2 / 2\sigma\mu_0\delta) (bd + ad + a^3/d + a^3b/d^2)$$

The quality factor is given by the total energy over the power dissipated over one period, or

$$Q = \omega U / P_t = abd(1 + d^2/a^2) / \delta (bd + ad + a^3/d + a^3b/d^2)$$

$$Q \sim 3 \cdot 10^4$$

Problem 5 G9.38

Putting boundaries in the z direction means that instead of propagating waves, there will be standing waves in that direction just like in the x and y directions. Thus the e^{ikz} in the expressions for the electric and magnetic fields in Eqn. 9.176 in Griffiths will have to be modified to $Ae^{ikz} + Be^{-ikz}$. Now, we know that the boundary conditions at the two ends in the z direction are

$$E_x = E_y = 0$$

and

$$B_z = 0$$

This immediately tells us that the z dependence of these quantities is of the form $\sin(kz)$ where

$$k = \frac{n\pi}{d}$$

for positive integers n . We can now write down the general expressions for the various components of the electric and magnetic fields inside the cavity. The electric field components are

$$\begin{aligned}\bar{E}_x(x, y, z, t) &= E_x(x, y) \sin(kz) e^{-i\omega t} \\ \bar{E}_y(x, y, z, t) &= E_y(x, y) \sin(kz) e^{-i\omega t} \\ \bar{E}_z(x, y, z, t) &= E_z(x, y) f_z(z) e^{-i\omega t}\end{aligned}$$

and the magnetic field components are

$$\begin{aligned}\bar{B}_x(x, y, z, t) &= B_x(x, y) g_x(z) e^{-i\omega t} \\ \bar{B}_y(x, y, z, t) &= B_y(x, y) g_y(z) e^{-i\omega t} \\ \bar{B}_z(x, y, z, t) &= B_z(x, y) \sin(kz) e^{-i\omega t}\end{aligned}$$

The dimensionless functions $f_z(z)$, $g_x(z)$ and $g_y(z)$ are all of the form $Ae^{ikz} + Be^{-ikz}$ and have to be determined from Maxwell's equations. Putting these into Maxwell's equations (iii) and (iv) of 9.177 in Griffiths, we get

$$\begin{aligned}\frac{\partial E_y(x, y)}{\partial x} - \frac{\partial E_x(x, y)}{\partial y} &= i\omega B_z(x, y) \\ \frac{\partial E_z(x, y)}{\partial y} - k \cos(kz) E_y(x, y) &= i\omega B_x(x, y) g_x(z) \\ -\frac{\partial E_z(x, y)}{\partial x} + k \cos(kz) E_x(x, y) &= i\omega B_y(x, y) g_y(z) \\ \frac{\partial B_y(x, y)}{\partial x} g_y(z) - \frac{\partial B_x(x, y)}{\partial y} g_x(z) &= -i\frac{\omega}{c^2} E_z f_z(z) \\ \frac{\partial B_z(x, y)}{\partial y} \sin(kz) - \frac{dg_y(z)}{dz} B_y(x, y) &= -i\frac{\omega}{c^2} E_x \sin(kz) \\ -\frac{\partial B_z(x, y)}{\partial x} \sin(kz) + \frac{dg_x(z)}{dx} B_x(x, y) &= -i\frac{\omega}{c^2} E_y \sin(kz)\end{aligned}$$

These equations are the resonant-cavity-equivalents of Eqn. 9.179 for wave guides in Griffiths and have to hold for all x, y and z inside the cavity. This immediately tells us from the second,

and

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which along with the above equations gives us

$$\bar{E}_x(x, y, z, t) = \frac{-iB_0\omega lmn(m\pi/b)}{(l\pi/a)^2 + (m\pi/b)^2} \cos(l\pi x/a) \sin(m\pi y/b) \sin(n\pi z/d) e^{-i\omega t}$$

$$\bar{E}_y(x, y, z, t) = \frac{iB_0\omega lmn(l\pi/a)}{(l\pi/a)^2 + (m\pi/b)^2} \sin(l\pi x/a) \cos(m\pi y/b) \sin(n\pi z/d) e^{-i\omega t}$$

$$\bar{B}_x(x, y, z, t) = \frac{-B_0(l\pi/a)(n\pi/d)}{(l\pi/a)^2 + (m\pi/b)^2} \sin(l\pi x/a) \cos(m\pi y/b) \cos(n\pi z/d) e^{-i\omega t}$$

$$\bar{B}_y(x, y, z, t) = \frac{-B_0(m\pi/b)(n\pi/d)}{(l\pi/a)^2 + (m\pi/b)^2} \cos(l\pi x/a) \sin(m\pi y/b) \cos(n\pi z/d) e^{-i\omega t}$$